

STABILITY OF INFINITE SLOPES

- In Fig. (a), X-X represents an infinite slope which is inclined to the horizontal at an angle β . On any plane YY (YY \parallel XX) at a depth z below the ground level the soil properties and the overburden pressure are constant. Hence, failure may occur along a plane parallel to the slope at some depth. The conditions for such a failure may be analysed by considering the equilibrium of the soil prism ABCD of width b .

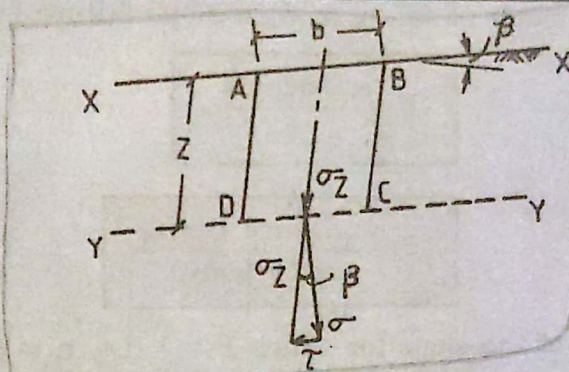


Fig (a)

Considering unit thickness, volume of the prism and, weight of the prism,

$$V = z b \cos\beta$$

$$W = \gamma z b \cos\beta$$

remember this figure

remember this

Vertical stress on YY due to self-weight,

$$\sigma_z = \frac{W}{b} = \gamma z \cos \beta \quad \dots(i)$$

This vertical stress can be resolved into the following two components:

$$\sigma = \sigma_z \cos \beta = \gamma z \cos^2 \beta \quad \dots(ii)$$

and,

$$\tau = \sigma_z \sin \beta = \gamma z \cos \beta \sin \beta \quad \dots(iii)$$

Failure will occur if the shear stress τ exceeds the shear strength τ_f of the soil. The factor of safety against such failure is given by.

$$F = \frac{\tau_f}{\tau} \quad \dots(iv)$$

(i) **Cohesionless soils** : from Coulomb's equation, we have

$$\tau_f = c + \sigma \tan \phi$$

For a cohesionless soil, $c = 0$,

$$\tau_f = \sigma \tan \phi$$

Substituting in eqn. (iv)

$$F = \frac{\sigma \tan \phi}{\tau}$$

Again, substituting the expressions for σ and τ .

$$F = \frac{\gamma z \cos^2 \beta \tan \phi}{\gamma z \cos \beta \sin \beta} = \frac{\tan \phi}{\tan \beta} \quad \dots(v)$$

When $\phi = \beta$, $F = 1$. Thus a slope in a cohesionless soil is stable till $\beta \leq \phi$, provided that no external force is present.

(ii) **c - ϕ soils**: In this case, the factor of safety against slope failure is given by,

$$F = \frac{c + \sigma \tan \phi}{\tau}$$

or

$$F = \frac{c + \gamma z \cos^2 \beta \tan \phi}{\gamma z \cos \beta \sin \beta} \quad \dots(vi)$$

Let H_c be the critical height of the slope for which $F = 1$ (i.e. $\tau_f = \tau$)

$$\therefore \gamma H_c \cos \beta \sin \beta = c + \gamma H_c \cos^2 \beta \tan \phi$$

or,

$$H_c = \frac{c}{\gamma \cos \beta (\sin \beta - \cos \beta \tan \phi)}$$

or,

$$H_c = \frac{c}{\gamma \cos^2 \beta (\tan \beta - \sin \phi)} \quad \dots(\text{vii})$$

Eqn. (vii) may also be written as:

$$\frac{c}{\gamma H_c} = \cos^2 \beta (\tan \beta - \tan \phi) \quad \dots(\text{viii})$$

or,

$$S_n = \cos^2 \beta (\tan \beta - \tan \phi) \quad \dots(\text{ix})$$

where,

S_n is a dimensionless quantity known as the stability number and is given by:

$$S_n = \frac{c}{\gamma H_c} \quad \dots(\text{x})$$

If a factor of safety F_c is applied to the cohesion such that the mobilised cohesion at a depth H is,

$$c_m = \frac{c}{F_c} \quad \dots(\text{xi})$$

Then,

$$S_n = \frac{c_m}{\gamma H} = \frac{c}{F_c \gamma H} \quad \dots(\text{xii})$$

γ may be γ_{sat} , γ_{sub}
or γ_{dry} depending upon
situation

From eqns. (x) and (xii), we get,

$$\frac{c}{\gamma H_c} = \frac{c}{F_c \gamma H}$$

or,

$$F_c = \frac{H_c}{H} = F_H$$

Hence, the factor of safety against cohesion, F_c , is the same as the factor of safety with respect to height, F_H .